





Automatique

PID controllers

Effects of proportional, integral and derivative terms

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These slides have been modified from an initial version developed by Quanser

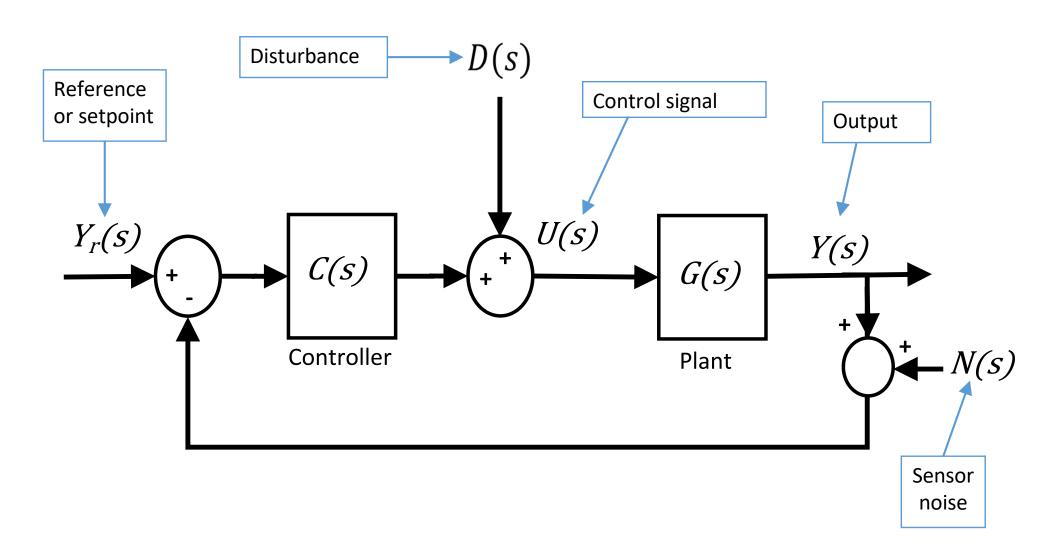
https://www.quanser.com

I sincerely thank Quanser for allowing me to adapt them





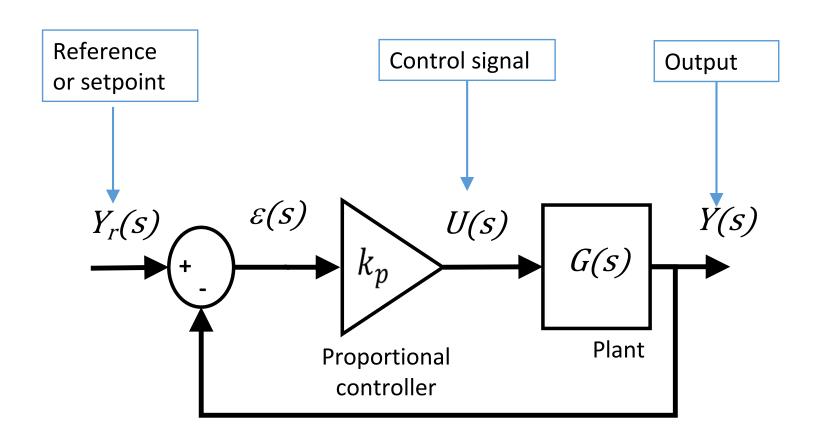
General feedback control diagram







Proportional Control







Equation of the P control law and transfer function

In the time domain:

In the Laplace domain:

$$u(t) = k_p \left(y_r(t) - y(t) \right)$$

$$u(t) = k_{p} \mathcal{E}(t)$$

$$U(s) = k_p \left(Y_r(s) - Y(s) \right)$$

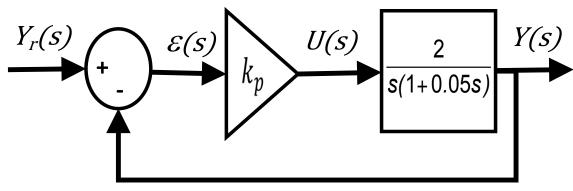
$$U(s) = k_p \mathcal{E}(s)$$

$$C(s) = \frac{U(s)}{\mathcal{E}(s)} = k_p$$

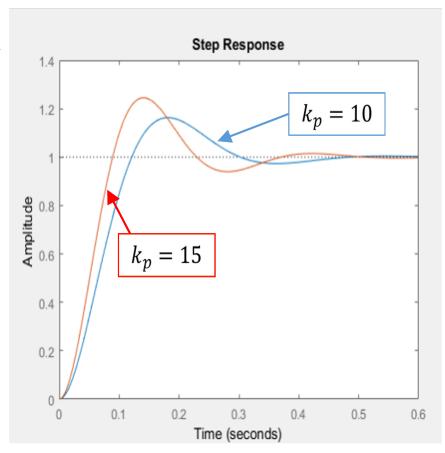




P control: effect of proportional gain



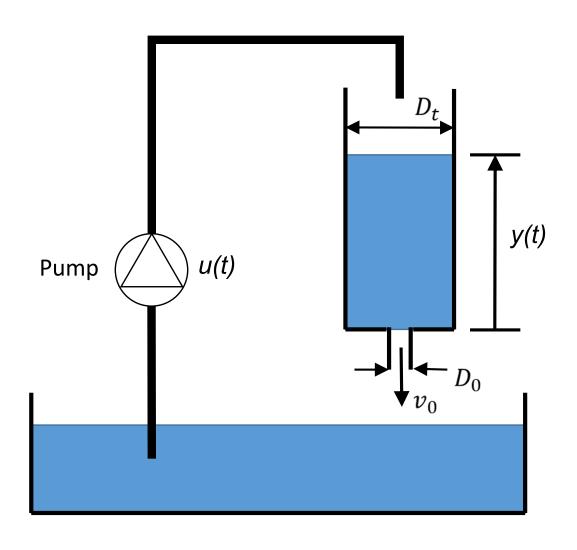
- Increase k_p gradually
- What can be noticed?
 - Peak time decreases, i.e. faster response
 - Overshoot increases







Example 1: water tank level control

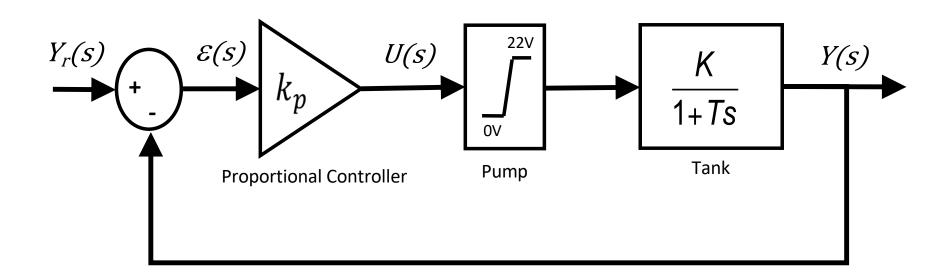


- Input: voltage sent to the pump u(t)
- Output : water level in the tank y(t)





Example 1: water tank level control



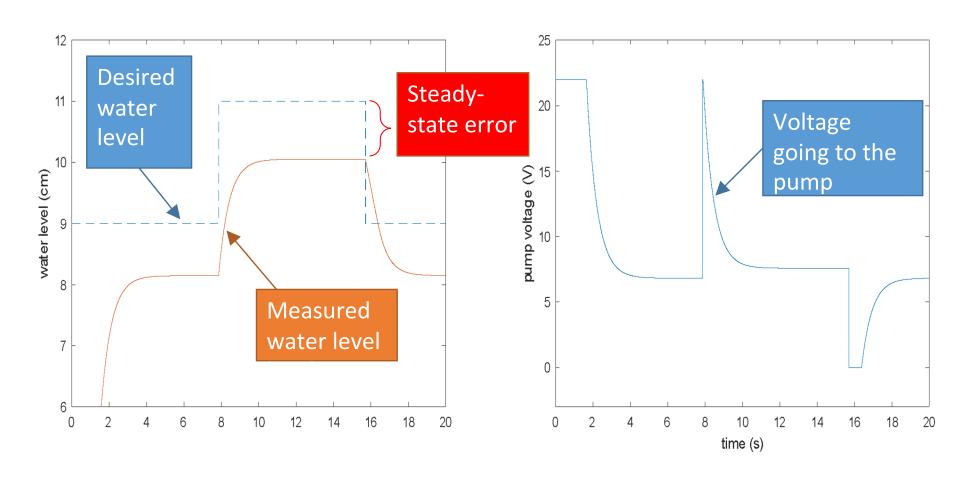




Response: water tank level P control

Tank response does not track desired water level well

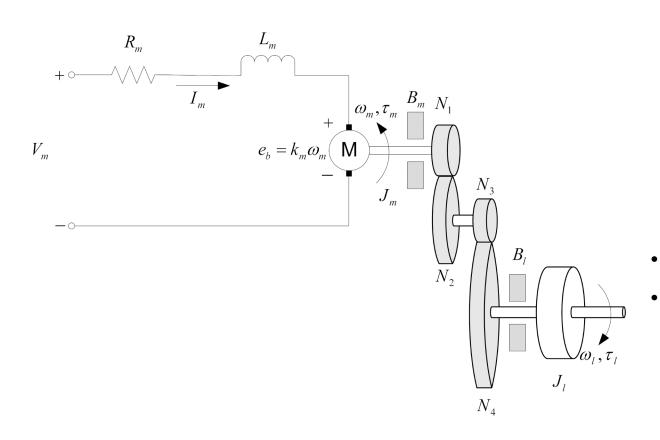
Control effort, i.e. voltage going to pump, is smooth







Example 2: P for servo motor position control



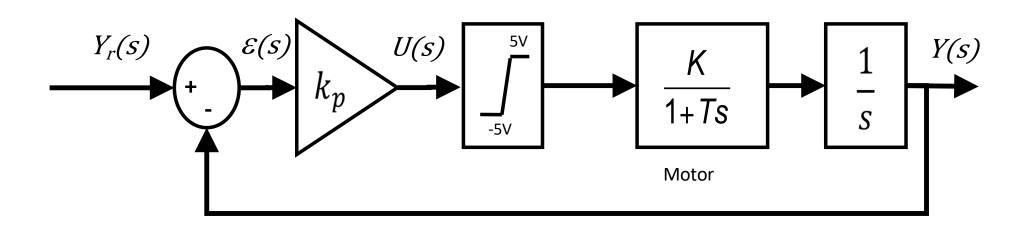


- Input: voltage sent to the motor *u(t)*
- Output : angular position y(t)





Example 2: P for servo motor position control



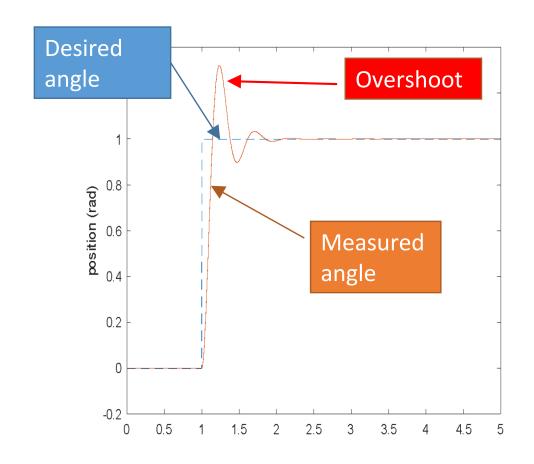


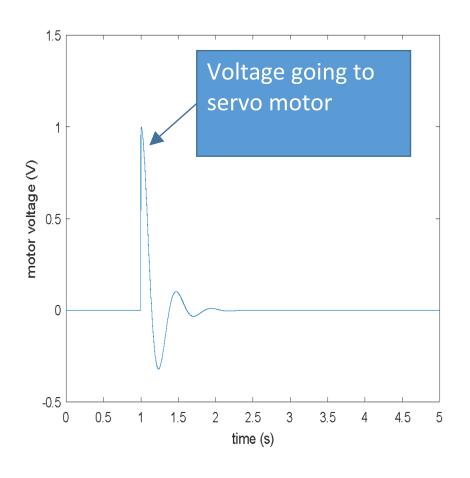


Response: P for servo motor position control

Servo response tracks desired servo angle well, but there is a large overshoot.

Control effort, i.e. voltage going to servo motor, is smooth









P control: take home message

Benefits

- Simple control
- "Good enough" for many systems
 - e.g. systems with an integrator in their plant

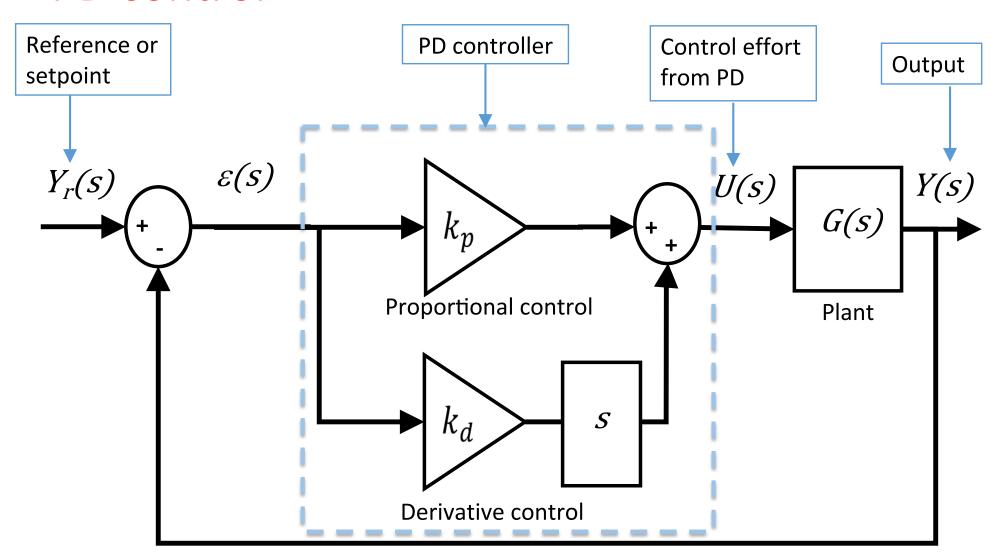
Drawbacks

- Can result in steady-state error
 - When plant has no integrator
 - When system has friction
- Can results in large overshoot





PD control



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Equation of the PD control law and transfer function

 $K_c = k_p$

 $T_d = \frac{k_d}{k}$

Parallel form

In the time domain:

$$u(t) = k_p \varepsilon(t) + k_d \frac{d\varepsilon(t)}{dt}$$

In the Laplace domain:

$$U(s) = \left(k_p + k_d s\right) \varepsilon(s)$$

$$C(s) = k_p + k_d s$$

 k_p is the proportional gain k_d is the derivative gain

In the time domain:

$$u(t) = K_c \left(\mathcal{E}(t) + T_d \frac{d\varepsilon(t)}{dt} \right)$$

In the Laplace domain:

$$U(s) = K_c \left(1 + T_d s \right) \mathcal{E}(s)$$

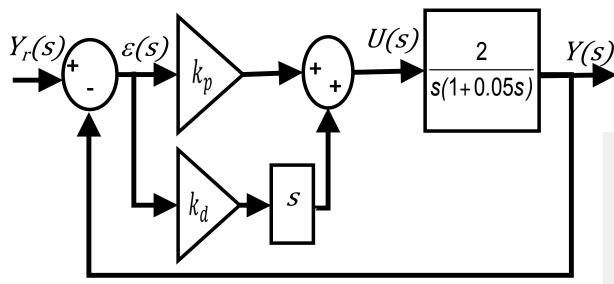
$$C(s) = K_c \left(1 + T_d s \right)$$

 K_c is the proportional gain T_d is the derivative time-constant

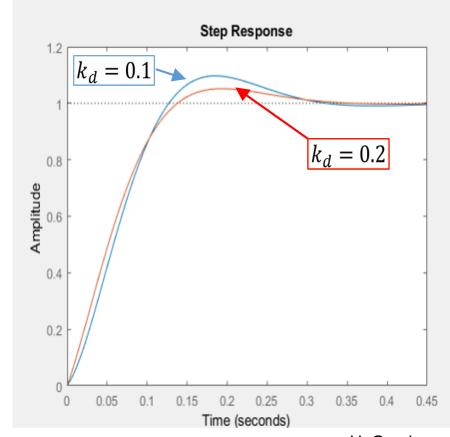




PD control: effect of derivative gain



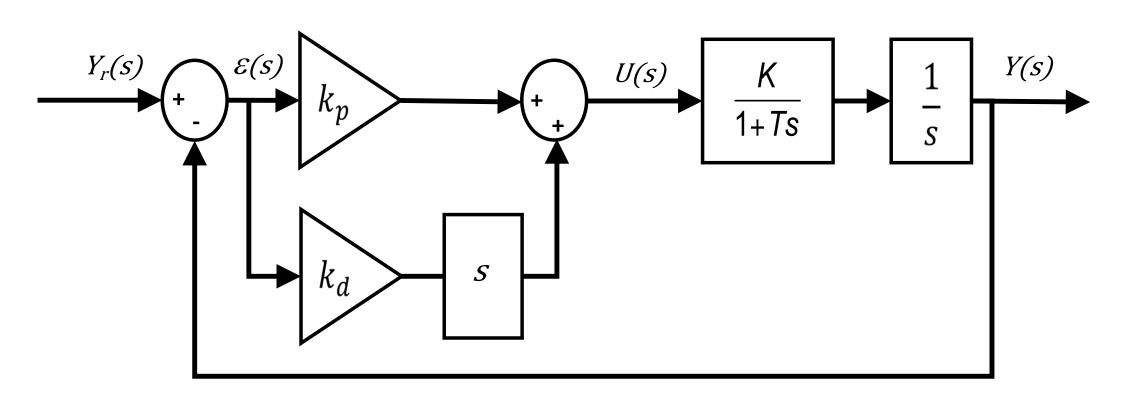
- Set $k_p = 10$
- Increase k_d gradually. What do you notice?
 - Overshoot decreases
 - Peak time increases, i.e. response slower







Example: PD for servo motor position control



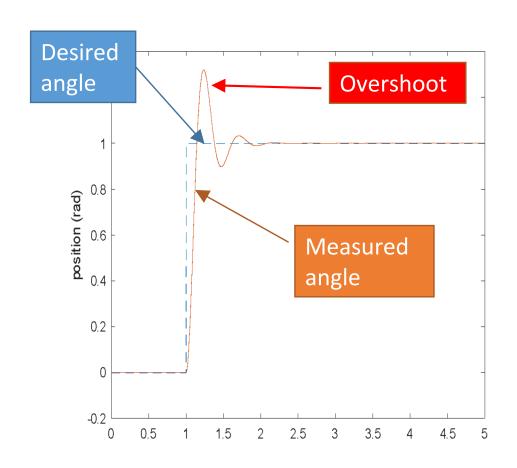


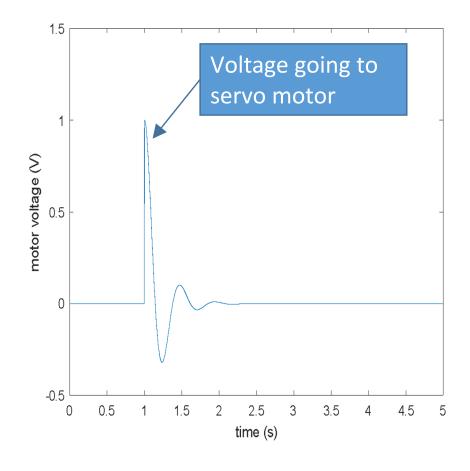


Recall: response with simple P servo control

Servo response tracks desired servo angle well, but there is a large overshoot

Control effort, i.e. voltage going to servo motor, is smooth





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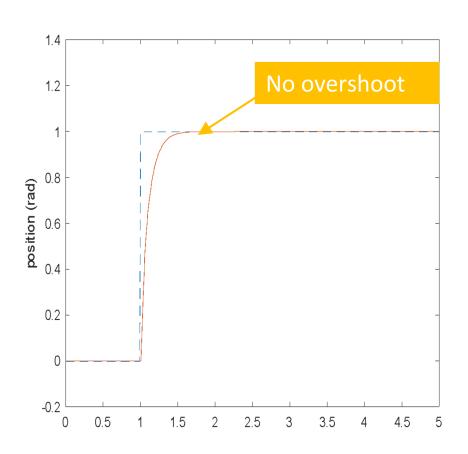


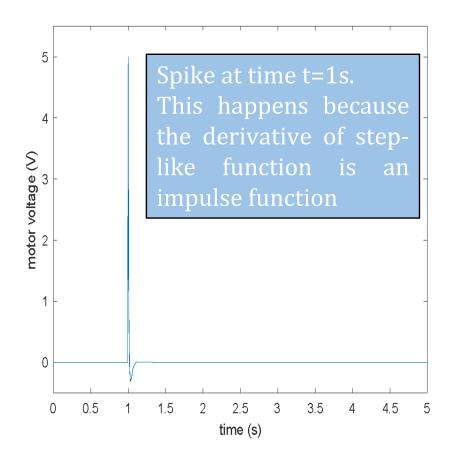


Now response with PD control

Adding derivative control lowers or removes the overshoot, but it slows down the response (i.e. increases peak/rise time)

Control effort, i.e. voltage going to servo, is smooth. But it is saturating the actuator at 5V





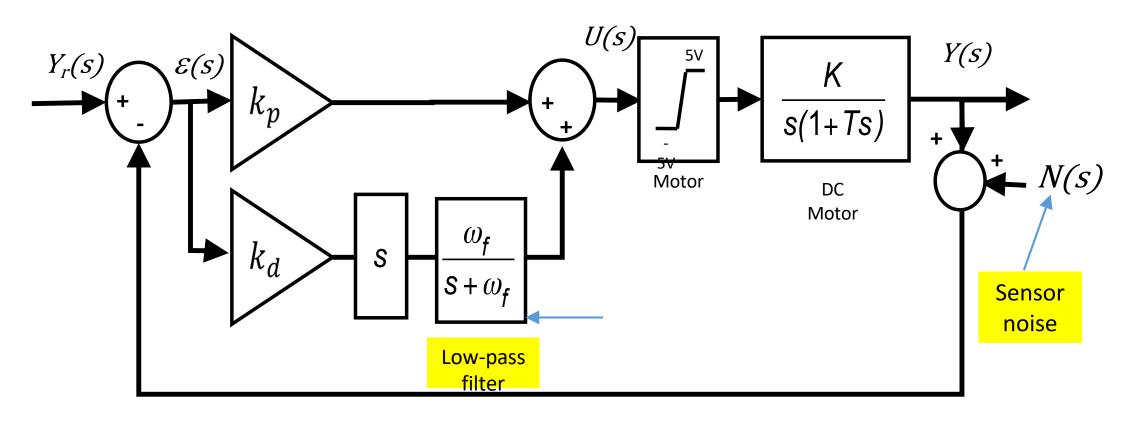




PD with low-pass filter

Goal of the filter: to reduce the effect of sensor noise

Example: PD with filtering for servo motor position control



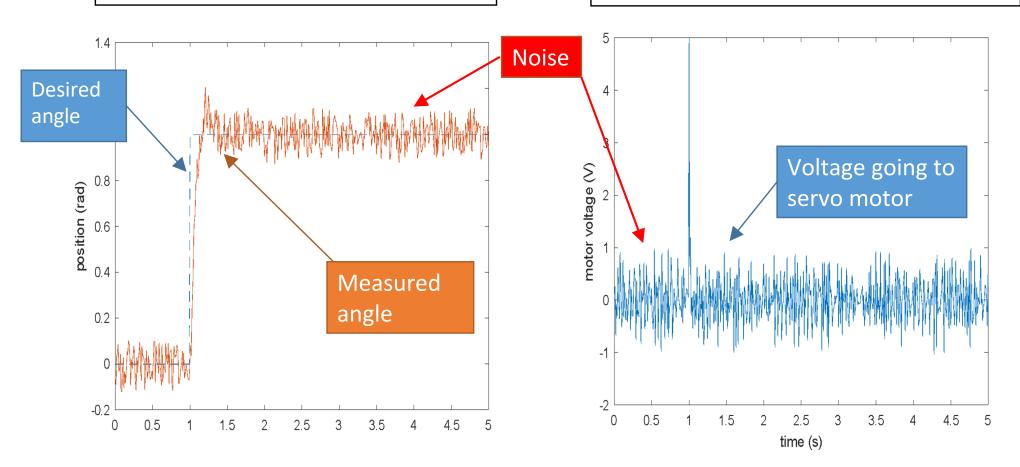




PD control with NO filtering



Control effort, i.e. voltage going to servo, is noisy

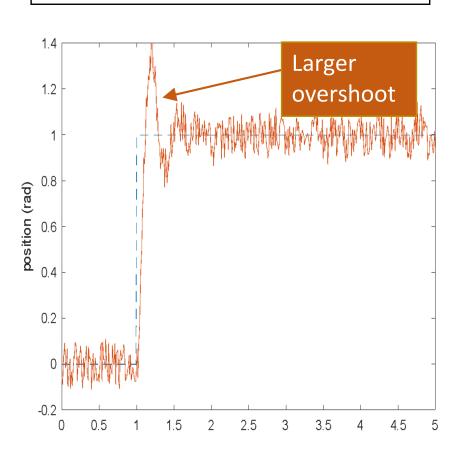




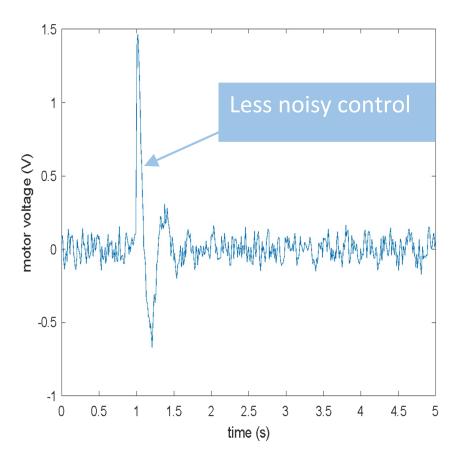


PD control with low-pass filtering

Adding filtering lowers noise, but it adds overshoot.



Control effort, i.e. voltage going to servo, is smoother (less noisy).

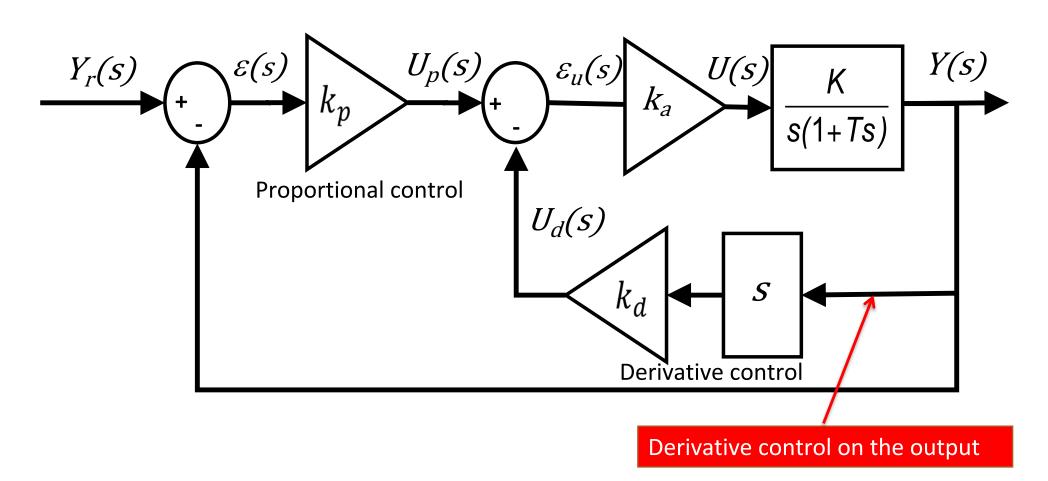






Variation of PD control

PD control with derivative effect on the output Goal: to avoid the spike effect after a step change on the setpoint







PD control: take home message

Benefits

- Removes overshoot
- Derivative plus low-pass filter can mitigate noisy output measurement effects
- Derivative control on the output to reduce the spike response after a setpoint step change

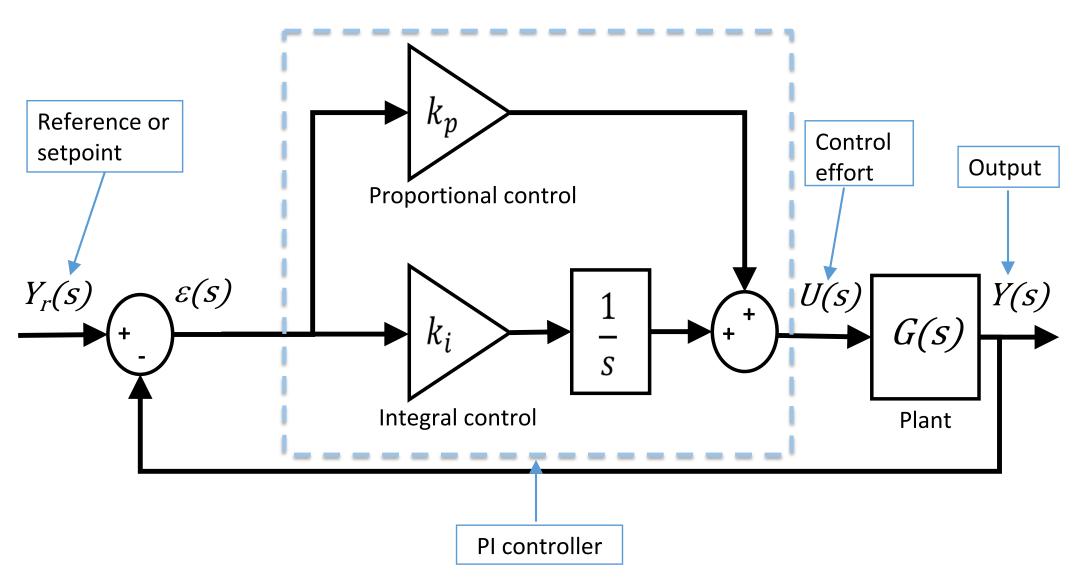
Drawbacks

- Can make output and control input noisy
 - e.g. due to sensor noise used in feedback
- Filtering slows down response and may result in overshoot





PI control







Equation of the PI control law and transfer function

 $K_c = k_p$

 $T_i = \frac{k_p}{k}$

Parallel form

In the time domain:

$$u(t) = k_p \varepsilon(t) + k_i \int_0^t \varepsilon(\tau) d\tau$$

In the Laplace domain:

$$U(s) = \left(k_p + \frac{k_i}{s}\right) \varepsilon(s)$$

$$C(s) = k_p + \frac{k_i}{s}$$

 k_p is the proportional gain k_i is the integral gain

In the time domain:

$$u(t) = K_c \left(\varepsilon(t) + \frac{1}{T_i} \int_{0}^{t} \varepsilon(\tau) d\tau \right)$$

In the Laplace domain:

$$U(s) = K_c \left(1 + \frac{1}{T_i s} \right) \mathcal{E}(s)$$

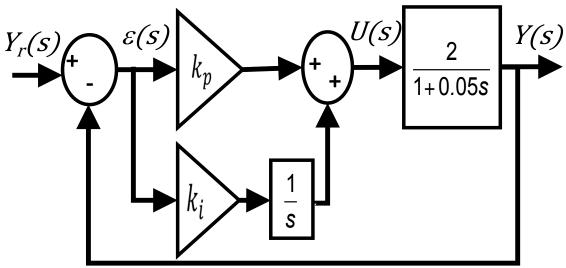
$$C(s) = K_c \left(1 + \frac{1}{T_i s} \right)$$

 K_c is the proportional gain T_i is the integral time-constant

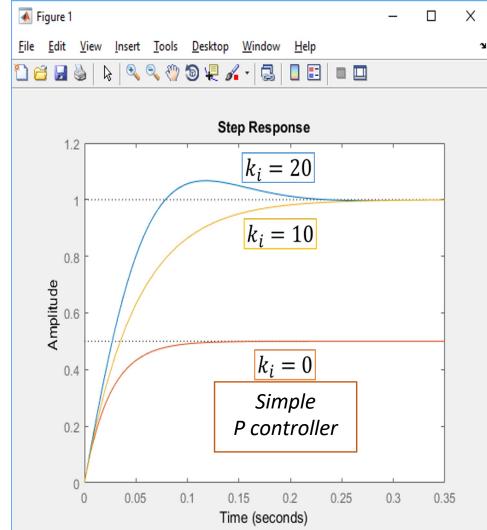




PI control: effect of integral gain



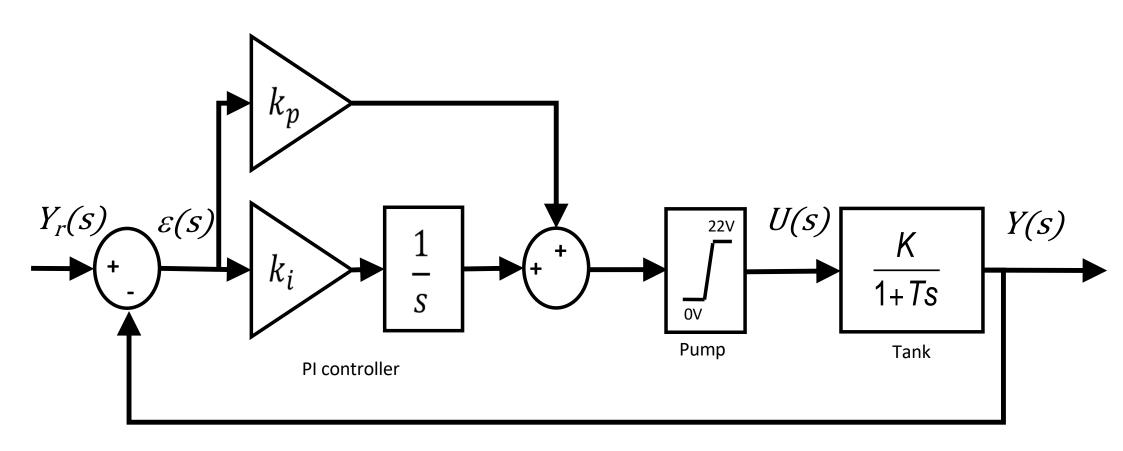
- Set $k_p = 0.5$
- Increase k_i gradually. What do you notice?
 - Steady-state error decreases
 - Response becomes faster, i.e. peak time decreases
 - Overshoot increases, i.e. response slows a bit







Example: tank level process control



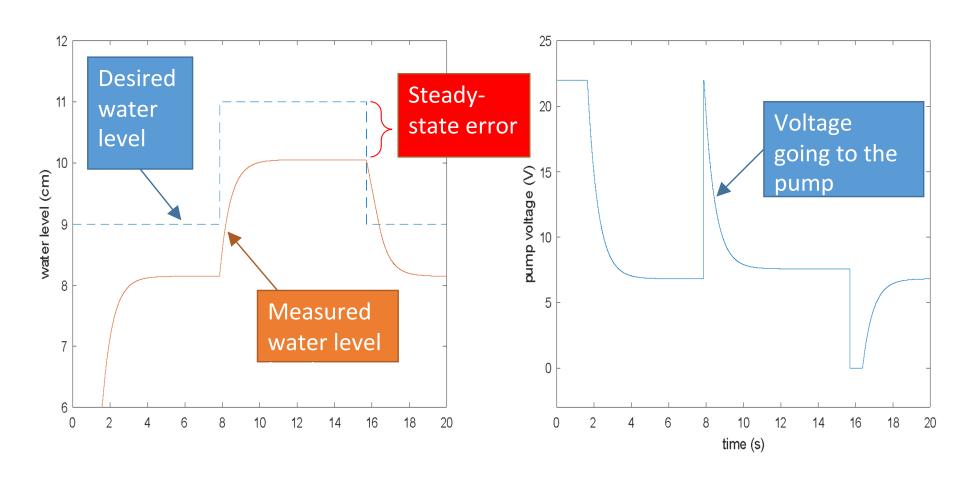




Recall the water tank level P control

Tank response does not track desired water level well

Control effort, i.e. voltage going to pump, is smooth



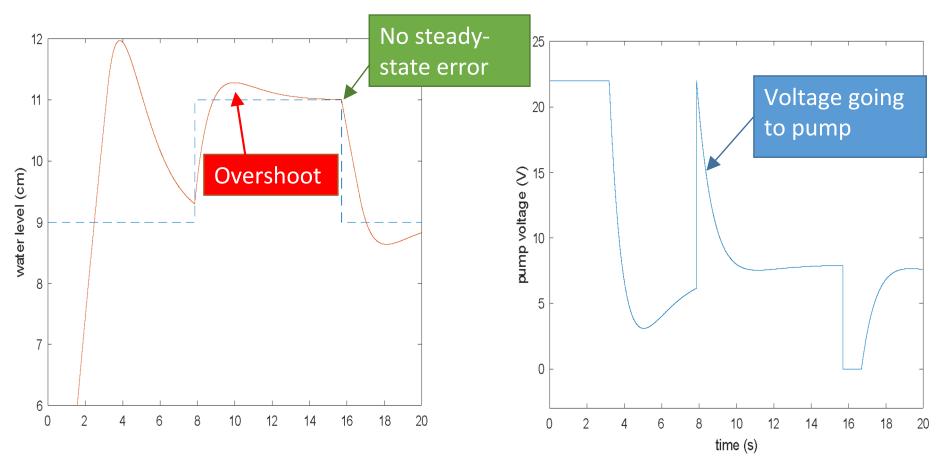




Water tank level PI control response

Tank response tracks desired water level well, but large overshoot

Control effort, i.e. voltage going to pump, is smooth but saturates actuator



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PI control: take home message

Benefits

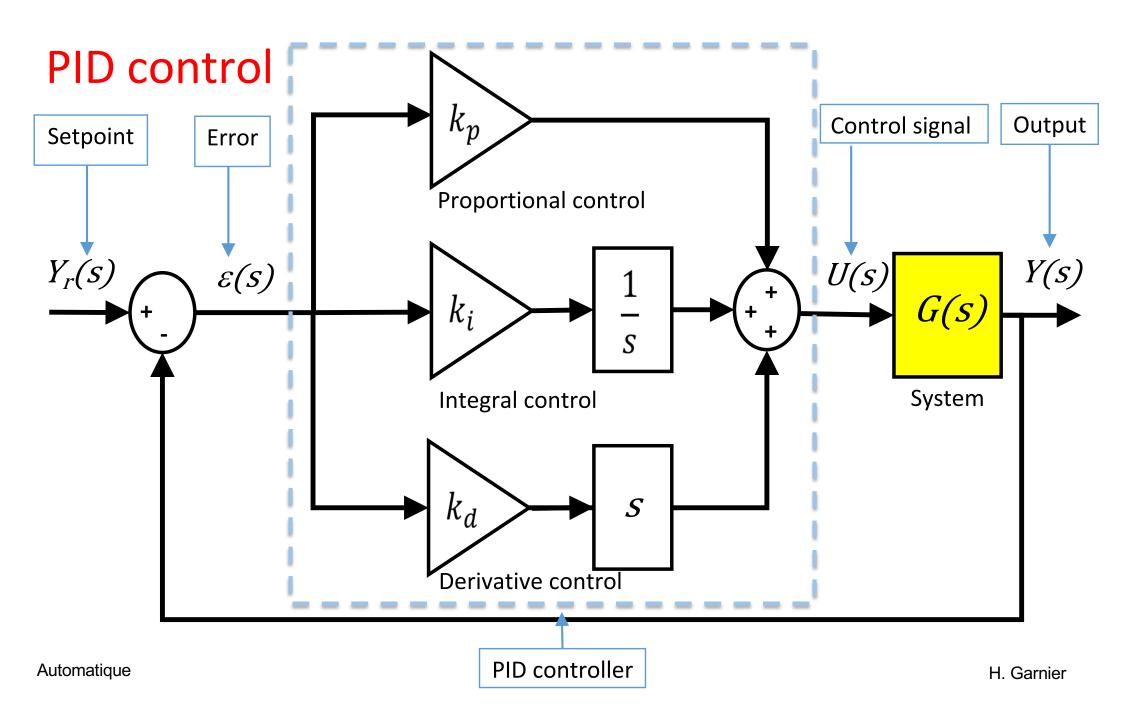
- Removes steady-state error
- Can reject disturbances

Drawbacks

- Can lead to large overshoot in response when control signal becomes saturated, i.e. "integral windup"
- Improperly designed integral gain can lead to instabilities







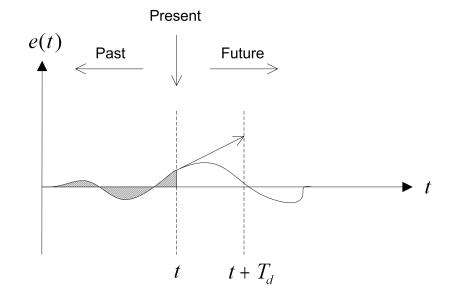


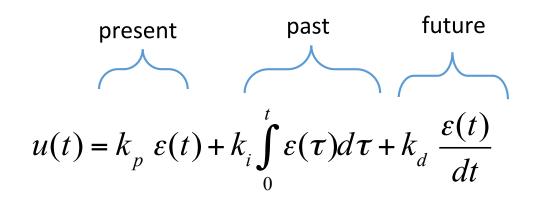


PID terms

To make corrective effects:

- k_p based on present error
- k_i depends on past error
- k_d prediction of future error









Equation of the PID control law and transfer function

 $T_d = \frac{k_d}{k}$

Parallel form

In the time domain:

$$u(t) = k_p \varepsilon(t) + k_i \int_0^t \varepsilon(\tau) d\tau + k_d \frac{\varepsilon(t)}{dt}$$

In the Laplace domain:

$$U(s) = \left(k_p + \frac{k_i}{s} + k_d s\right) \varepsilon(s)$$

$$C(s) = k_p + \frac{k_i}{s} + k_d s$$

 k_p is the proportional gain k_i is the integral gain k_d is the derivative gain

In the time domain:

$$u(t) = K_c \left(\varepsilon(t) + \frac{1}{T_i} \int_{0}^{t} \varepsilon(\tau) d\tau + T_d \frac{\varepsilon(t)}{dt} \right)$$

In the Laplace domain:

$$U(s) = K_c \left(1 + \frac{1}{T_i s} + T_d s \right) \mathcal{E}(s)$$

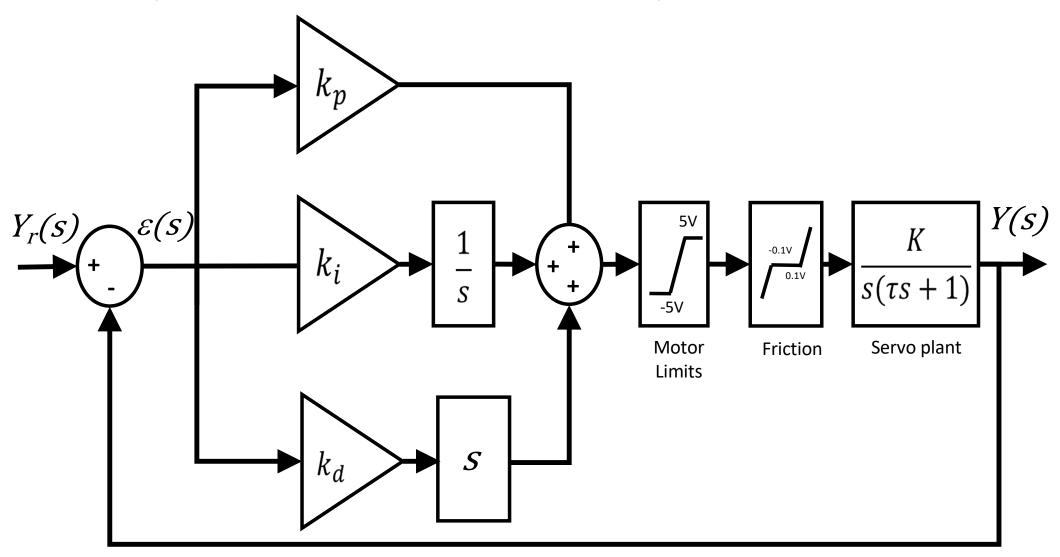
$$C(s) = K_c \left(1 + \frac{1}{T_i s} + T_d s \right)$$

 K_c is the proportional gain T_i is the integral time-constant T_d is the derivative time-constant





Example: PID for servo motor position control



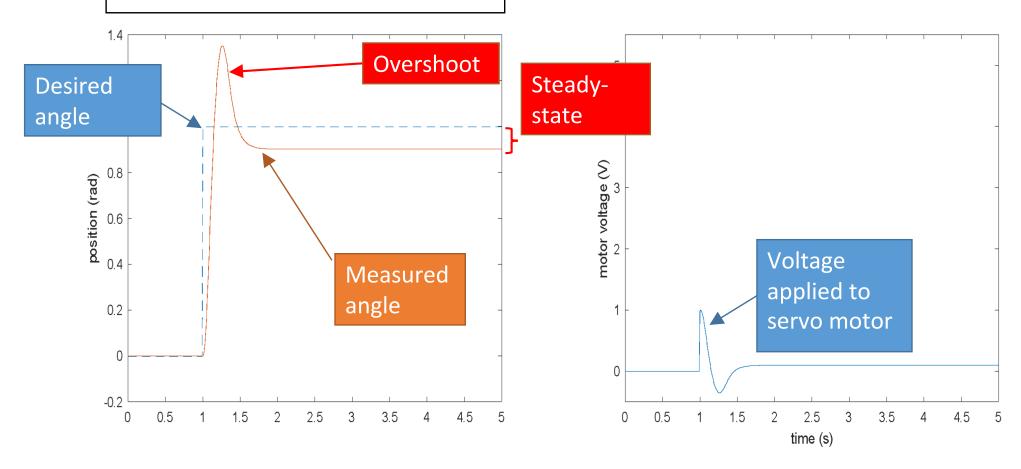




Response with simple P control

Servo response tracks desired servo angle well, but there is a large overshoot and steady-state error (due to friction).

Control effort, i.e. voltage going to servo, is smooth



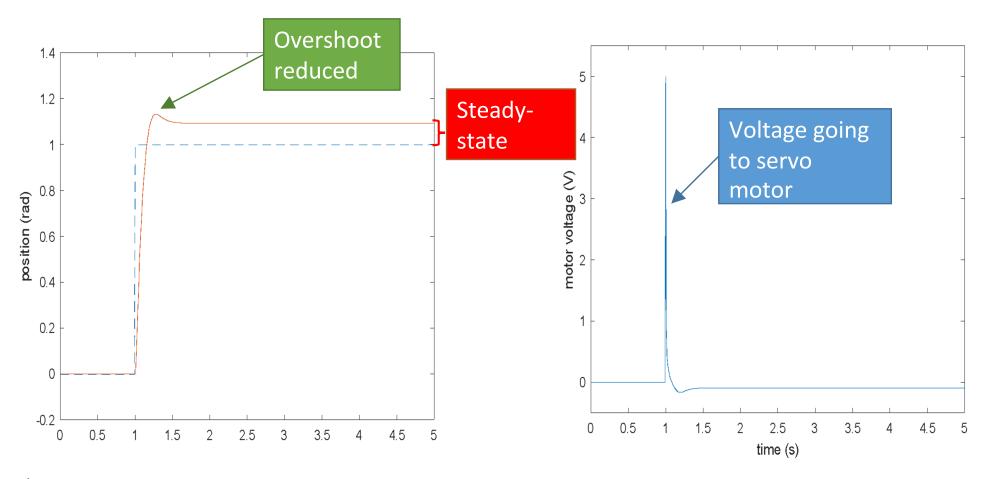




Response with PD control

Servo response tracks desired servo angle well, overshoot is reduced, but there is a steady-state error.

Control effort, i.e. voltage going to servo, is smooth. But it is saturating the actuator at 5V.



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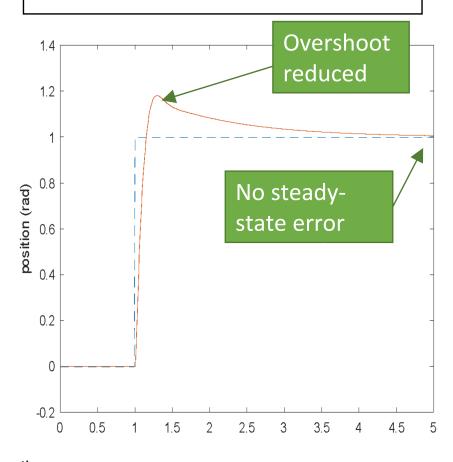


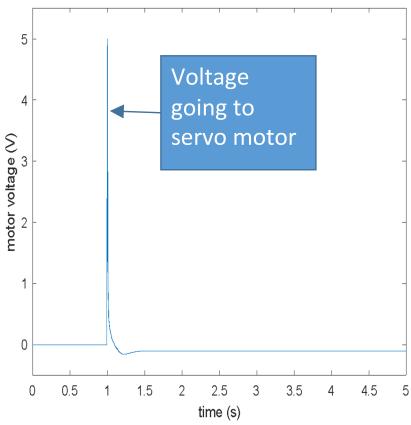


Response with PID control

Servo response tracks desired servo angle well, overshoot is reduced, and steady-state error has been removed.

Control effort, i.e. voltage going to servo, is smooth. But it is saturating the actuator at 5V.





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Practical form of PID controller used in the industry

$$C(s) = K_c \left(1 + \frac{1}{T_i s} + T_d s \right) = K_c \left(\frac{T_i T_d s^2 + T_i s + 1}{T_i s} \right)$$

Some controllers, in particular old PID version have a proportional band (PB) setting instead of a controller gain K_c

 $PB = \frac{100}{K_c}$ $C(s) = \frac{100}{PB} \left(1 + \frac{1}{T_i s} + T_d s \right)$

where *PB* is the proportional mode and is defined as, "the percentage error that results in a 100% change in controller output"

The derivative term causes the gain to increase without bound as frequency goes up. Practical PID controllers limit this high frequency gain with a first-order low pass filter. A practical PID controller form is then the following

$$C(s) = K_c \left(\frac{T_i T_d s^2 + T_i s + 1}{T_i s} \right) \left(\frac{\omega_f}{s + \omega_f} \right) \quad \frac{2}{T_d} \le \omega_f \le \frac{10}{T_d}$$





Summary: what do PID terms do?

Advantage

- Proportional (P)
 - Speeds up response
- Derivative (D)
 - Decreases overshoot
- Integral (I)
 - Cancels steady-state error
 - Rejects disturbance

Disadvantage

- Proportional (P)
 - Increases overshoot
- Derivative (D)
 - > Slows down response
- Integral (I)
 - Slows down response







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Practical aspects of PID controllers Anti-windup strategy

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Version du 28 novembre 2024

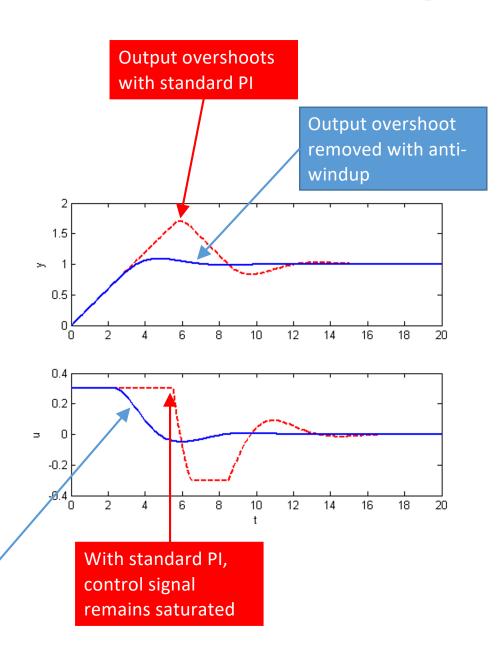




Integral Windup Effect

- When the control signal becomes saturated, the integrator keep outputting a control signal to compensate for the error
 - Output reaches setpoint at t = 4
 - ... but integrator has stored so much energy, it overshoots
 - Control signal goes down only at t = 6

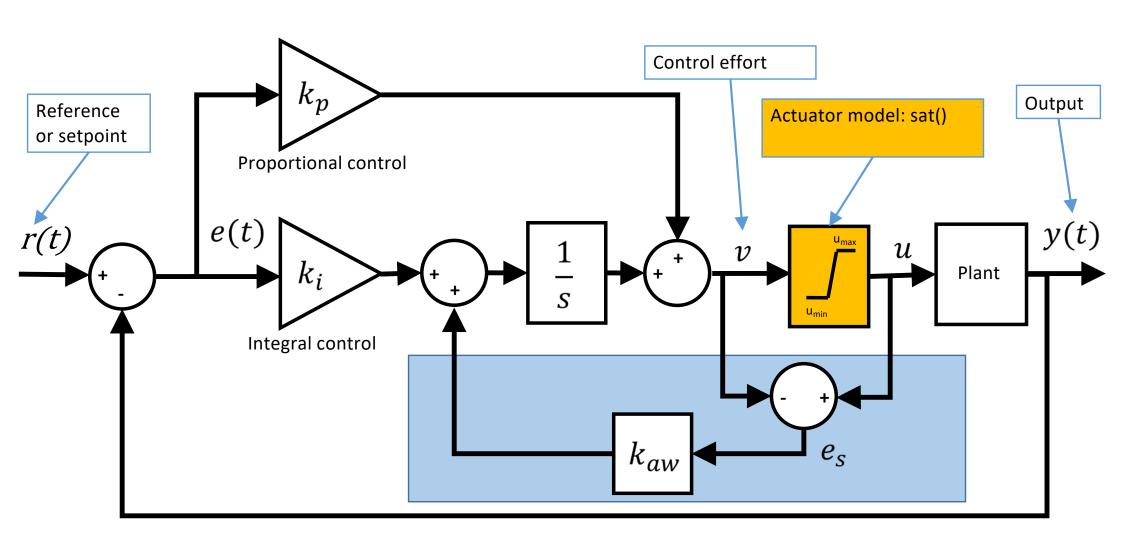
Control signal goes down with anti-windup







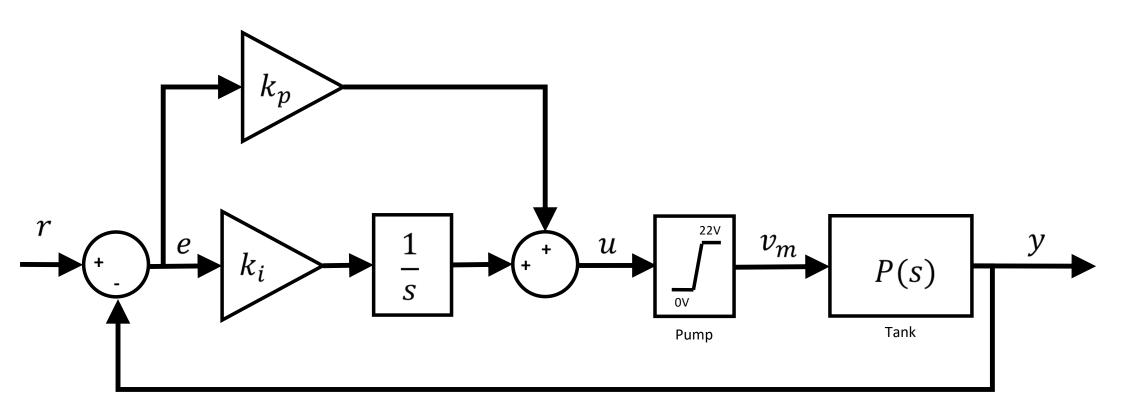
PI Feedback Loop with Integral Anti-Windup







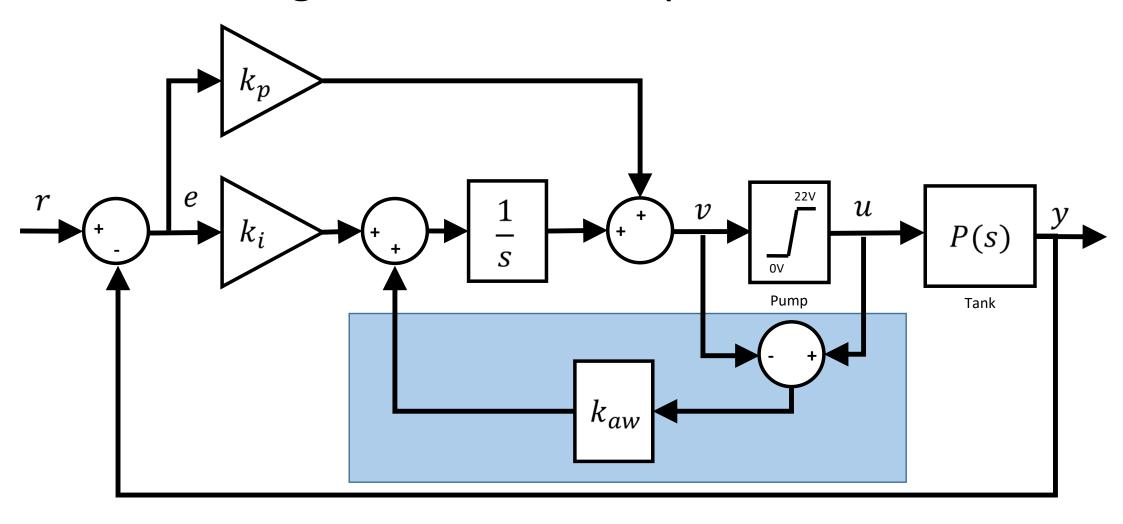
Tank Level Process Control – without Anti-Windup







With Integrator Anti-Windup



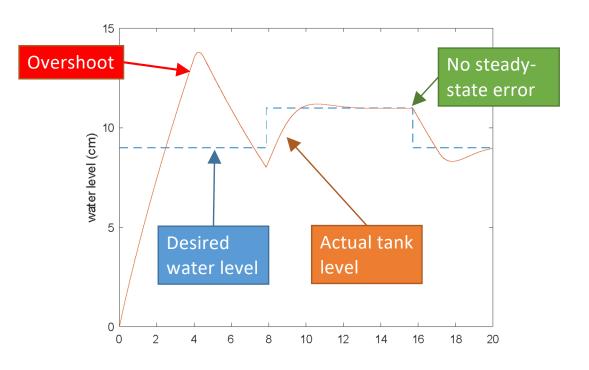


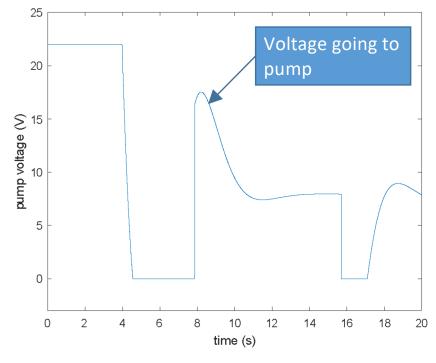


Recall: PI Control Response (without anti-windup)

Tank response tracks desired water level well, but large overshoot

Control effort, i.e. voltage going to pump, is smooth but saturates actuator





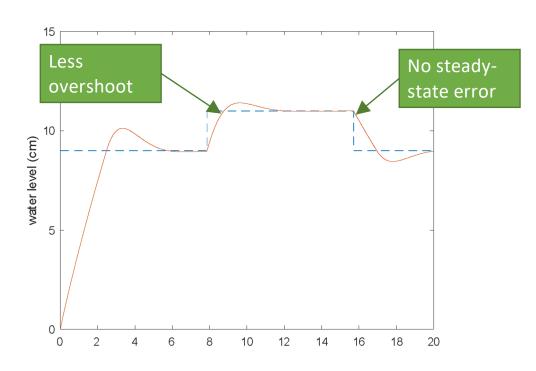


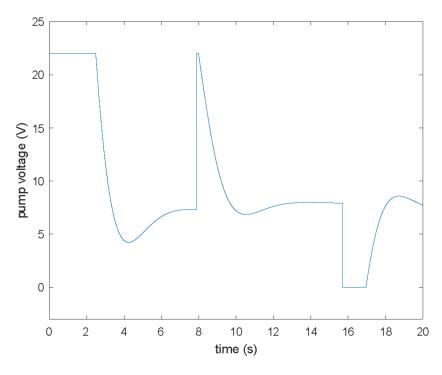


PI + Anti-Windup Control Response

Tank response tracks desired water level well and now has less overshoot

Control effort, i.e. voltage going to pump, is smooth. It still saturates the actuator, but less then before

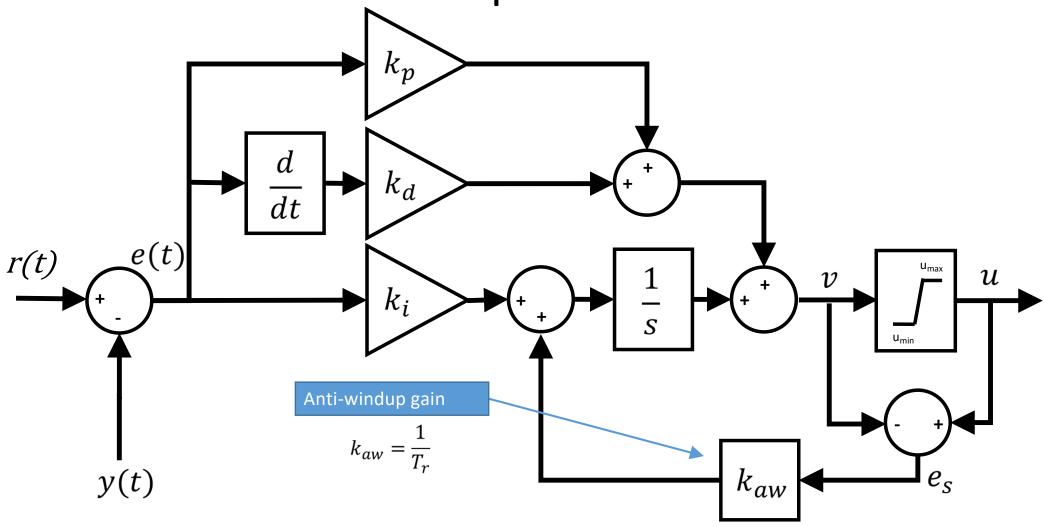








PID with Anti-Windup







Anti-Windup Gain Design

Anti-windup gain is commonly defined with respect to a **reset time** T_r

$$k_{aw} = \frac{1}{T_r}$$

- Short reset time (large gain) integral reset more quickly
- Long reset time (small gain) integral is reset more slowly
- Caution: Setting T_r too small can lead to undesirable reset when measurement noise is present





Anti-Windup Gain Design

Reasonable compromise is to select a reset time that is a fraction of the integral and derivative time.

$$T_r = \sqrt{T_i T_d}$$

Or with respect to the anti-windup gain

$$k_{aw} = 1/T_r = \frac{1}{\sqrt{T_i T_d}}$$

Parameterized PID equation (commonly used in industry):

$$u(t) = k \left(e(t) + \frac{1}{T_i} \int_0^t e(\tau) d\tau + T_d \frac{de(t)}{dt} \right)$$

where k is the proportional gain, T_i is the integral time, and T_d is the derivative time

In the time-domain:

$$u(t) = k_p e(t) + k_i \int_0^t e(\tau) d\tau + k_d \frac{de(t)}{dt}$$





Takeaways – PID with Anti-Windup

Benefits

- Removes steady-state error like PI
- Can reject disturbances like PI
- Removes undesirable overshoot
- More robust

Drawbacks

- Actuator is still saturated, but this helps
- More complicated to implement